

# A pathway towards the use of fossil fuels for power generation and transportation

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creating tomorrow's infrastructure... **sustainably**

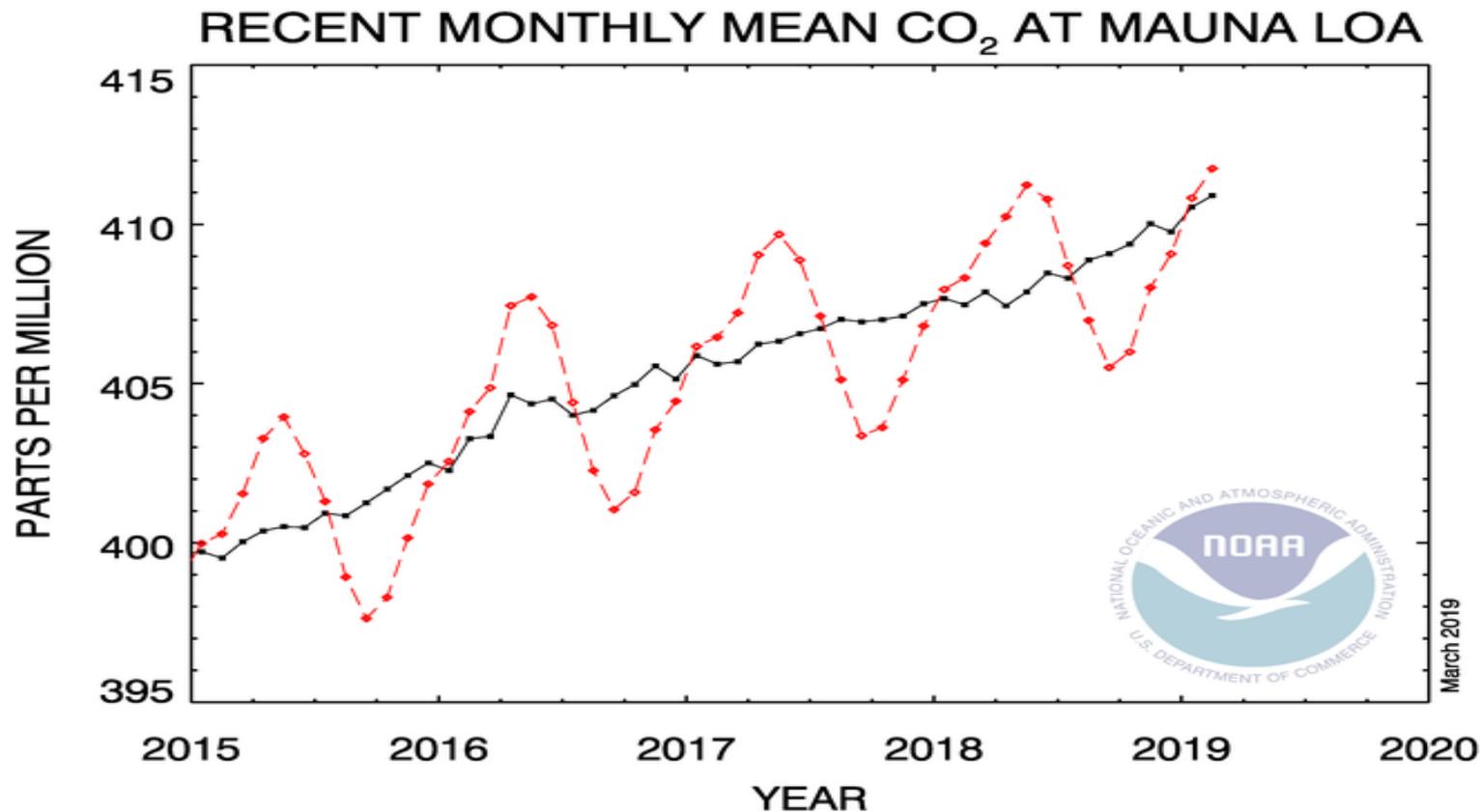
# Summary of the talk

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- Background
- Development of the Allam Cycle
- Detailed design considerations
- Equipment needed
- Demonstration plant
- Hydrogen production
- Hydrogen fuel for vehicles
- OXY-FUEL conversion of existing coal fired power stations.coal fired power stations
- CONTINUING USE OF FOSSIL FUELS WITH 100% CO<sub>2</sub> CAPTURE IS POSSIBLE

# CO<sub>2</sub> level in the atmosphere

## Continuing increase in atmospheric CO<sub>2</sub> levels from fossil fuels

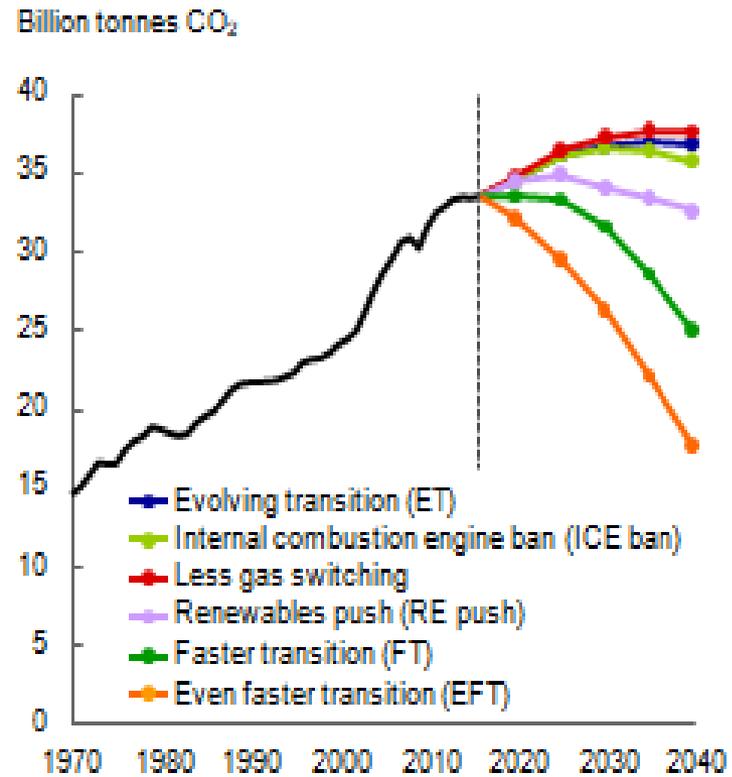
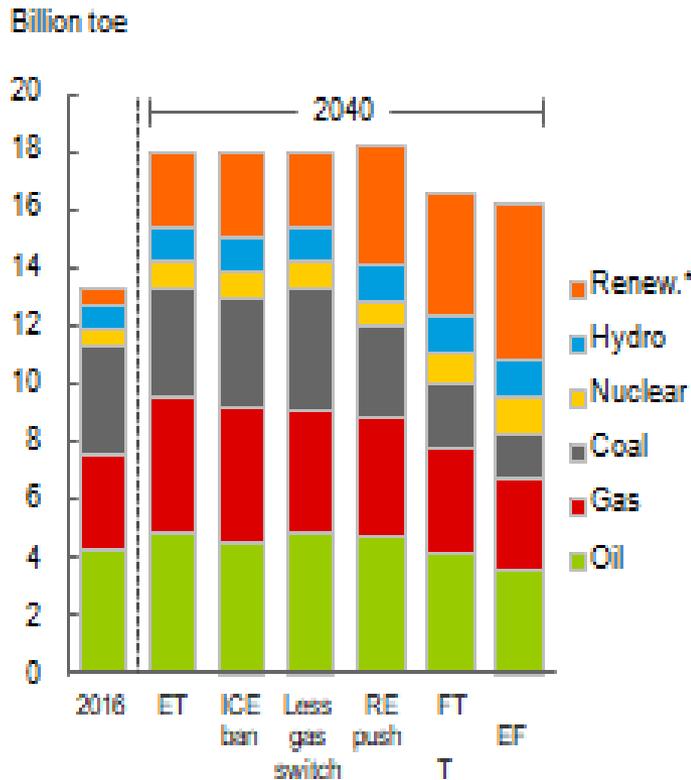




# The Energy Outlook considers a range of scenarios...

Primary energy consumption by fuel

Carbon emissions

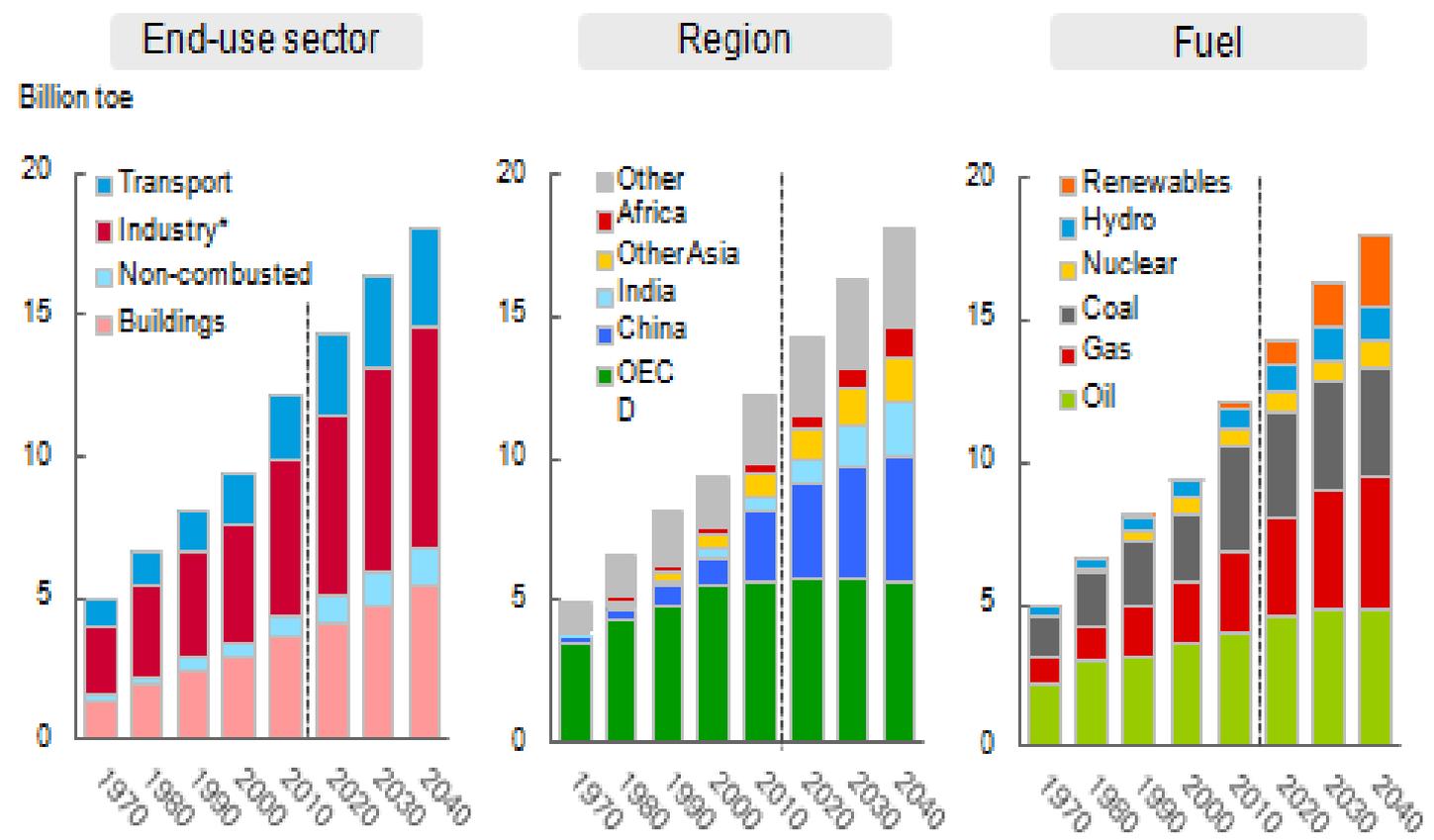


\*Renewables includes wind, solar, geothermal, biomass, and biofuels  
For full list of data definitions see p122



# The Outlook examines the energy transition...

## Primary energy demand

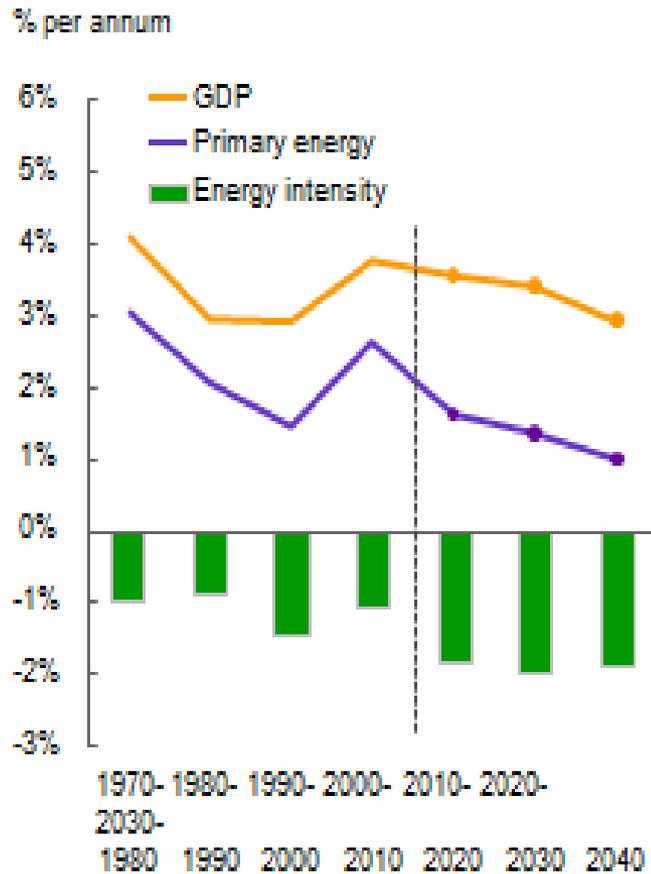


\*Industry excludes non-combusted use of fuels

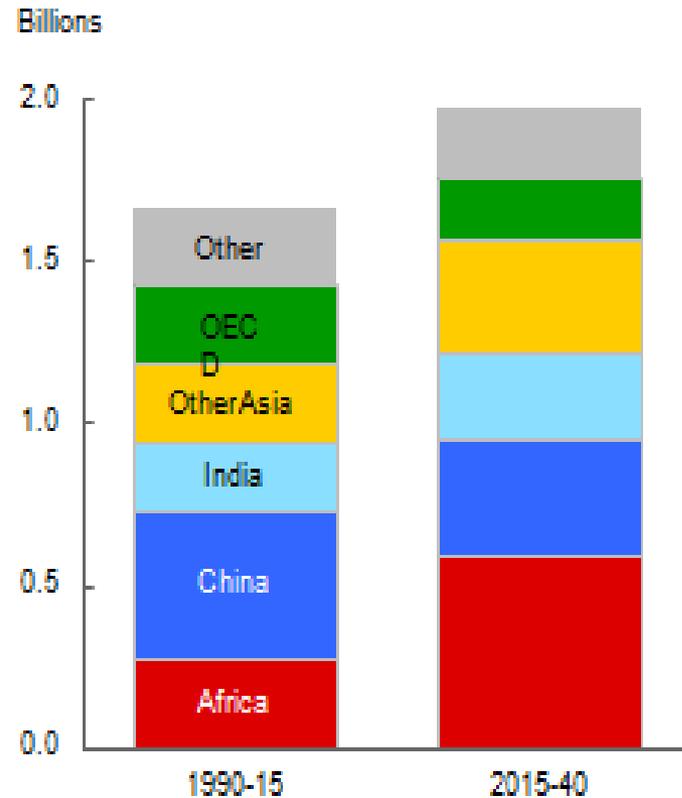


# Increasing global prosperity drives growth in energy demand...

### Growth in GDP and primary energy



### Growth in urban population by region

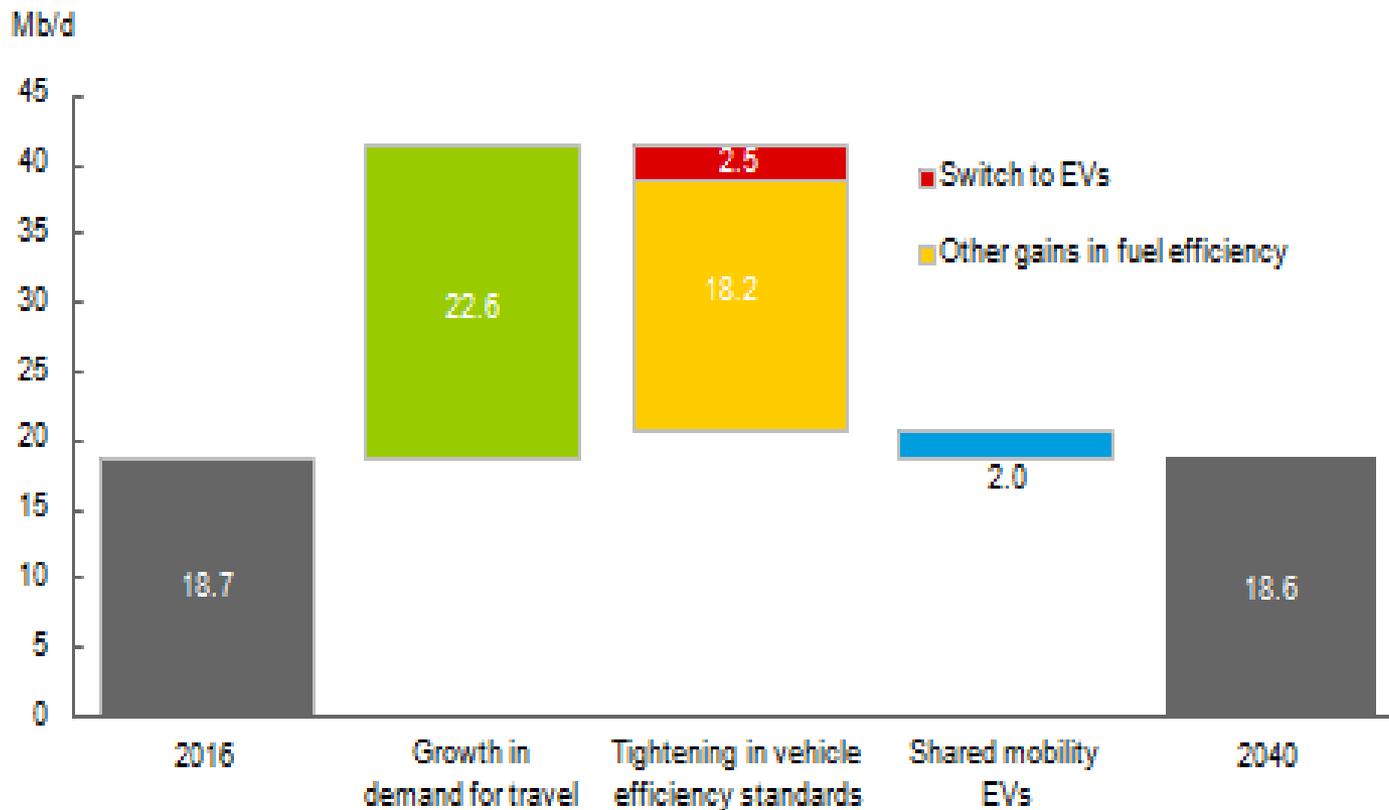


2018 BP Energy Outlook  
© BP p.l.c. 2018



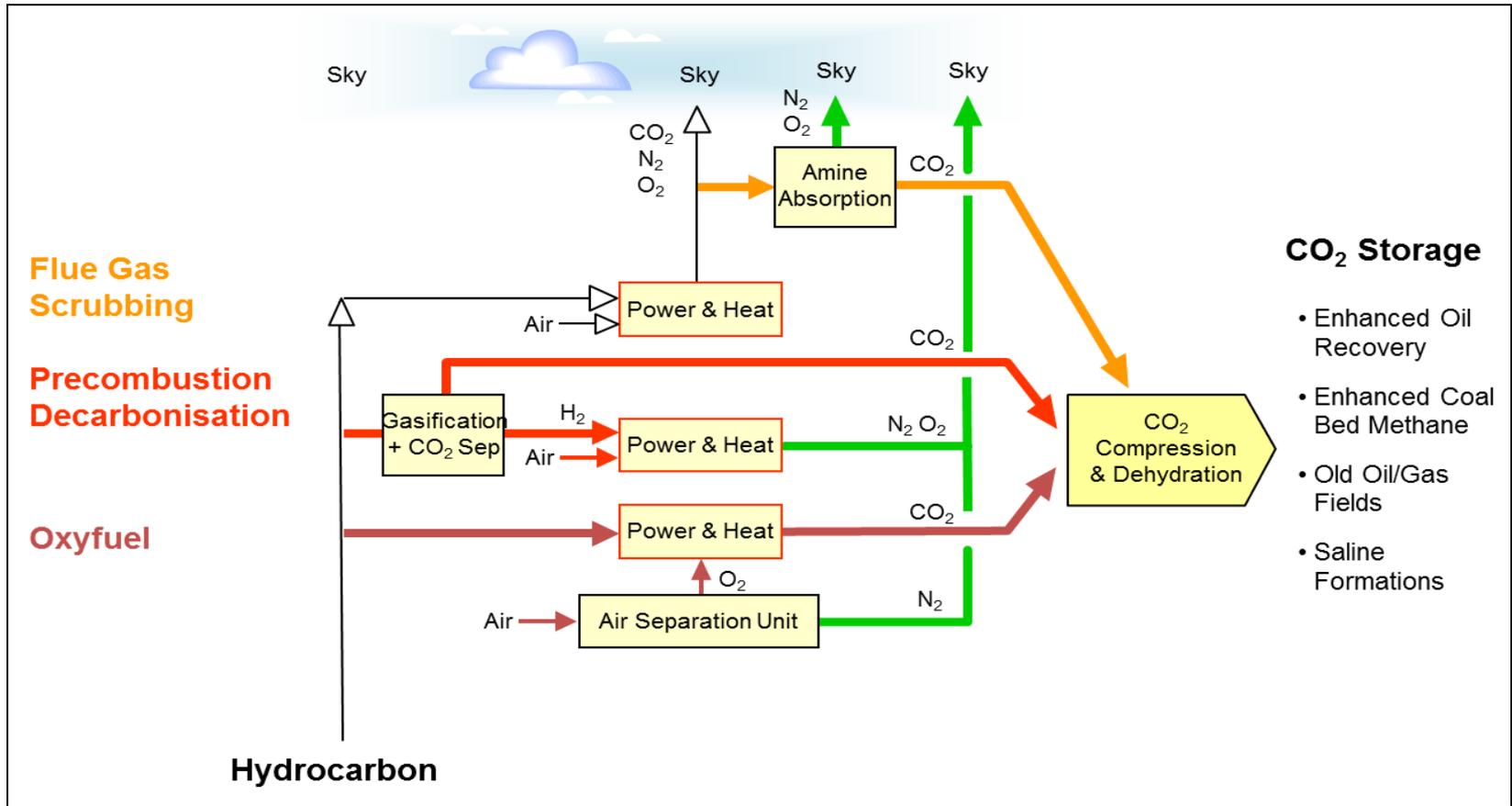
# Liquid fuel use in cars is broadly flat...

## Changes in liquids demand from cars: 2016-2040



# CURRENT OPTIONS FOR CLEAN FOSSIL FUEL POWER PRODUCTION

ALL lead to a 50% to 70% increase in electricity costs



# What is the Allam Cycle?

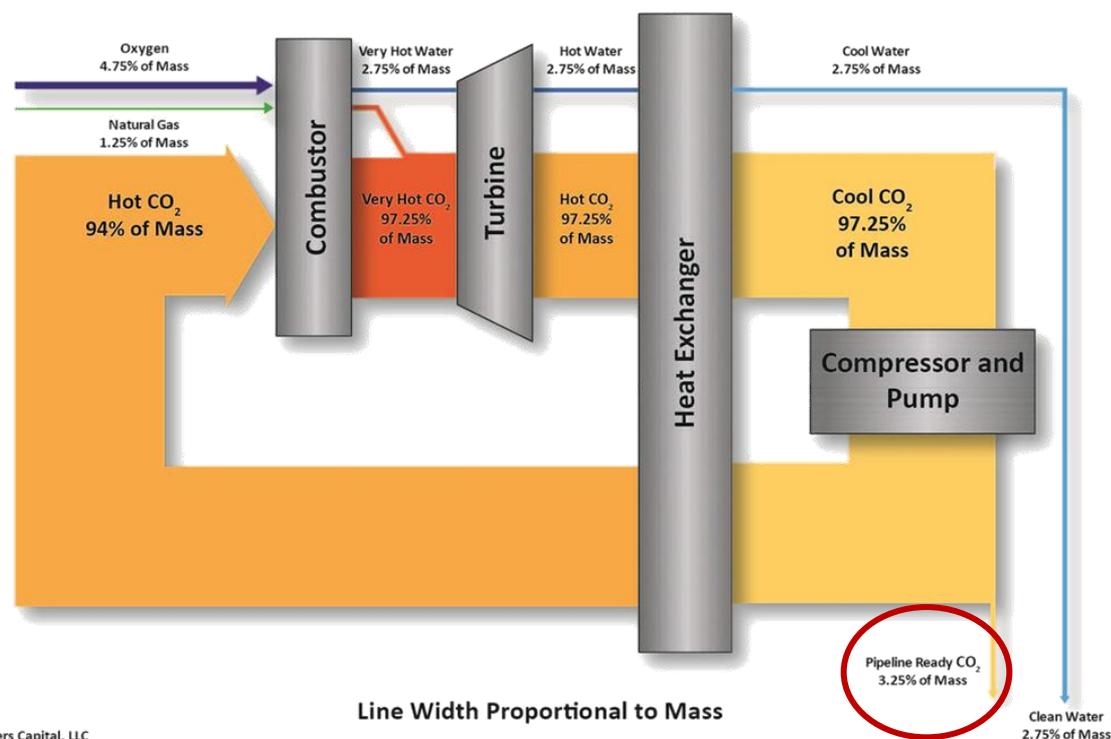
- **The Allam Cycle is**

- A semi-closed, supercritical CO<sub>2</sub> Brayton cycle,
- That uses oxy-combustion with natural gas, gasified coal, or other carbonaceous fuels.

- **Historically, CO<sub>2</sub> capture has been expensive, whether using air to combust or oxy-combustion.**

- **The Allam Cycle makes oxy-combustion economic by:**

- Relying on a more efficient core power cycle.
- Recycling heat within the system to reduce O<sub>2</sub> and CH<sub>4</sub> consumption, and associated costs of the ASU.





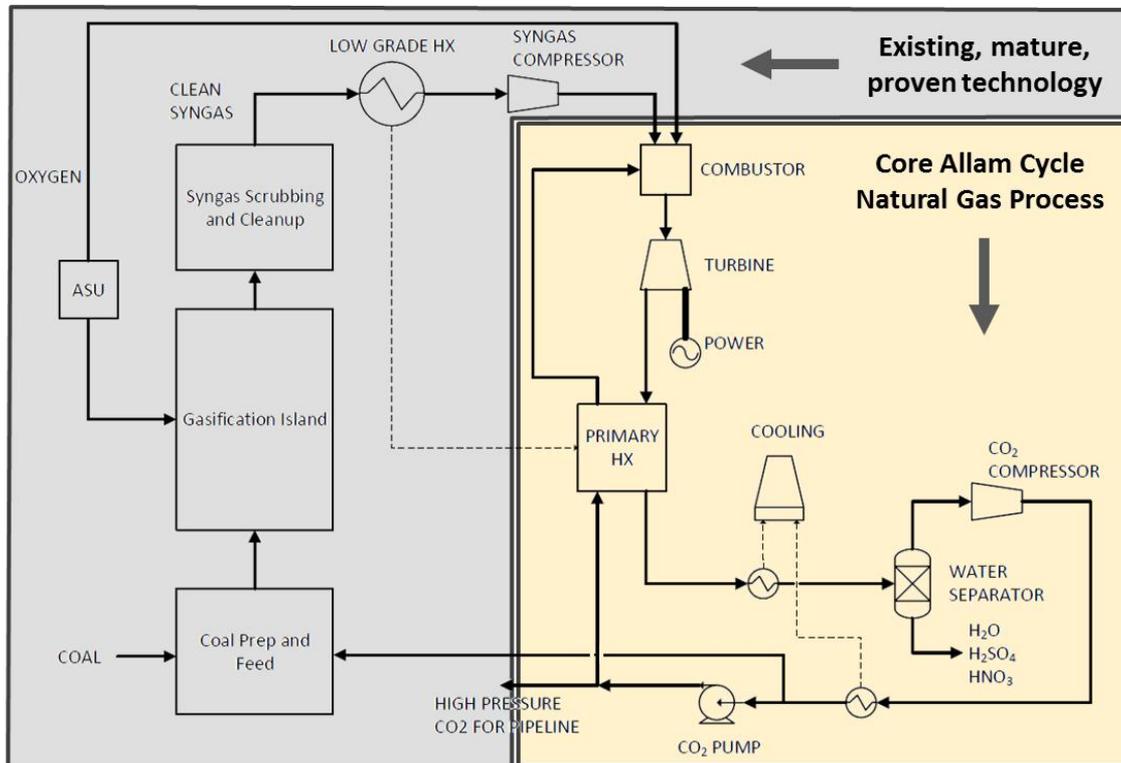


# ECONOMICS OF POWER PRODUCTION USING NATURAL GAS

	<b>NET Power</b>	<b>Combined Cycle (without carbon capture)</b>	<b>Combined Cycle with Carbon Capture</b>
<b>Efficiency</b> <small>(portion of energy of gas vs. energy of produced electricity)</small>	57% (1150°C)	55% to 62%	38% to 51%
<b>Percent of CO<sub>2</sub> Captured</b>	100%	0%	85%
<b>NO<sub>x</sub> emissions (lb/MWh)</b>	0	0.025-0.026	0.025-0.026
<b>“Levelized” cost of electricity without CO<sub>2</sub> revenues (\$/MWh)</b>	\$62.9 to \$69.4	\$64.0 to \$72.8	\$91.6 to \$134.2
<b>“Levelized” cost of electricity with CO<sub>2</sub> revenues (\$/MWh) at \$20/ton</b>	\$55.5 to \$62.0	\$64.0 to \$72.8	\$85.6 to \$128.3

# Allam Cycle for Coal or Waste Hydrocarbon Fuels

The Allam Cycle can be used with a range of solid fuels while maintaining the benefits of the core cycle.



Efficiency	LHV	HHV
Gross Turbine Output	76.3%	72.5%
Coal prep & feed	-0.2%	-0.2%
ASU	-10.2%	-9.7%
CO <sub>2</sub> , Syngas Comp.	-9.1%	-8.7%
Other Auxiliaries	-6.5%	-6.1%
<b>Net Efficiency</b>	<b>50.3%</b>	<b>47.8%</b>

- Lowest cost electricity from coal with 100% CO<sub>2</sub> at 28bar to 300bar taken directly from the CO<sub>2</sub> recycle compression.
- All impurities are removed from the coal gas prior to combustion or as H<sub>2</sub>SO<sub>4</sub> and HNO<sub>3</sub> after combustion.
- Most of the sensible heat in the cleaned coal gas plus steam following water quench is recovered at fuel value in the Allam cycle; directly improving efficiency.
- Process simplification significantly reduces cost vs. IGCC

## Other Applications of the Allam Cycle using natural gas

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Countries which import LNG can heat the compressed LNG to pipeline temperature and liquefy the ambient temperature turbine exhaust eliminating the CO<sub>2</sub> compressor and increasing the effective efficiency of a 1000Mw power station to about 66% (LHV basis)

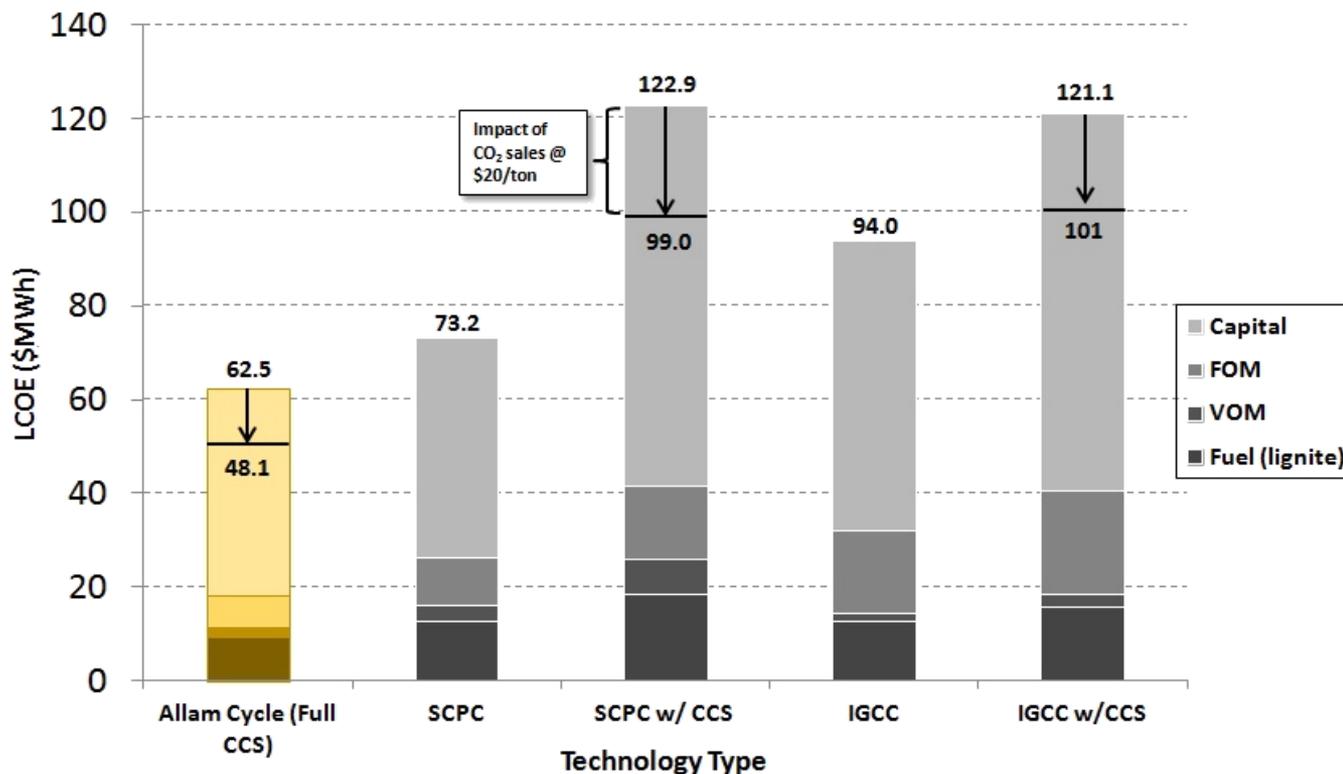
Steam from a supercritical coal fired boiler at typically 300bar and 600°C can be superheated to 720°C in the recuperator heat exchanger giving a large increase in the coal power station efficiency and capturing 100% of the CO<sub>2</sub> produced from the additional fuel required to superheat the steam.

CO<sub>2</sub> captured at typically 150bar pipeline pressure can be injected into oil wells for enhanced oil recovery. Associated natural gas separated from the oil which will contain a large quantity of CO<sub>2</sub> can be used directly as fuel for the Allam cycle power system allowing efficient capture and recycling of the CO<sub>2</sub>.

Natural gas containing say 25 mol% H<sub>2</sub>S can be used as fuel in the Allam cycle. We have developed an effective H<sub>2</sub>S removal technology applicable to both natural gas and coal derived POX gas

CO<sub>2</sub> captured can be used for enhanced coal bed CH<sub>4</sub> production.

# Increased Performance, Lower Capex, Reduced Complexity Lead to Much Lower LCOE Projections for Allam Cycle Coal



## Reduction in costs from removal of:

~~Steam turbine  
HRSG  
Steam piping/equipment  
Water-gas shift reactor  
High Temp syngas cooler  
NO<sub>x</sub> control unit/SCR unit~~

## Potential removal of:

AGR/sulfur recovery unit  
COS hydrolysis  
Solvents/catalysts

### Notes

- Lu et al. Oxy-Lignite Syngas Fueled Semi-Closed Brayton Cycle Process Evaluation (2014)
- Total Plant Cost and O&M costs were estimated for lignite-fired system in conjunction with EPRI; AACE Class 5 estimate
- Cost data for other technologies is taken from NETL baseline reports (Vol. 3, 2011)

# NET Power's Is Demonstrating the Allam Cycle process

## 50MWth gas plant in La Porte, TX

- Scaled down from 500MWth design
- Construction nearing completion; commissioning in progress.

## Includes all core components

- Combustor/turbine, heat exchangers, pumps/compressors, controls, etc.
- Grid connected and fully operable

## \$140 million (USD) program

- Includes first of a kind engineering, all construction, and testing period
- Partners include Exelon Generation, CB&I, 8 Rivers and Toshiba



# Technical Development of the NET Power Demonstration Plant

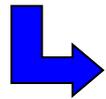
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- McDermott (CB&I) led detailed design, procurement and construction and is designing the commercial plant.
- Exelon operate the facility.
- 8 Rivers has provided the proprietary process design, dynamic simulation, and control philosophy with ongoing development.
- Toshiba has developed the novel turbine and combustor.
- The demonstration main process heat exchanger is supplied by Heatric.
- Oxygen is supplied via pipeline from an adjacent Air Liquide ASU.

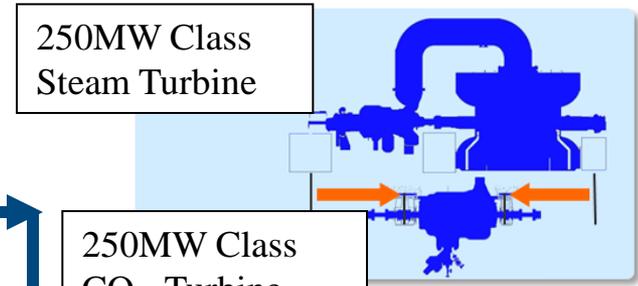
# Technology for supercritical CO<sub>2</sub> Turbine

## Gas Turbine Technology

1300-1500°C



Working fluid; CO<sub>2</sub>  
Pressure; 2MPa ⇒ 30MPa

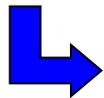


250MW Class  
Steam Turbine

250MW Class  
CO<sub>2</sub> Turbine

## Combustor Technology

1300-1500°C



Working fluid; CO<sub>2</sub>  
Pressure; 2MPa ⇒ 30MPa



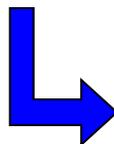
Turbine & Combustor for  
Super Critical CO<sub>2</sub> Cycle  
Temp. 1150°C  
Press. 30MPa

## Steam Turbine Technology

USC& A-USC

Pressure; 24-31MPa

Temperature; 600-750°C

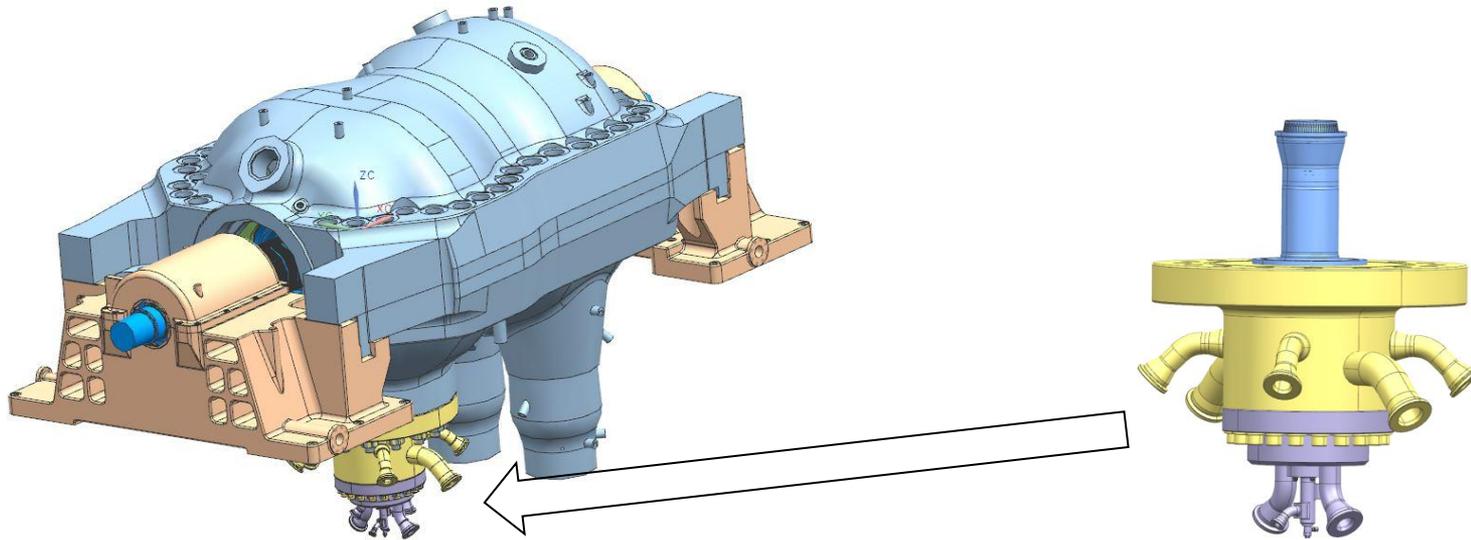


Temperature ⇒ 1150°C



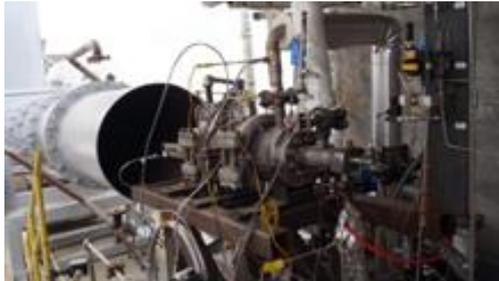
# 50MWth Combustor

1. First of a kind in view of high pressure and working fluid.
2. Stable diffusion flame can be used since there is no NOx emission.
3. No need of using innovative cooling scheme since temperature is within experience of existing gas turbine.
4. Rig test in order to validate operation has been completed.



Combustor for Demonstration Plant

# The Toshiba Turbine and Combustor (cont.)



*Left: Test stand for a 5 MWth combustor operating at 300bar*

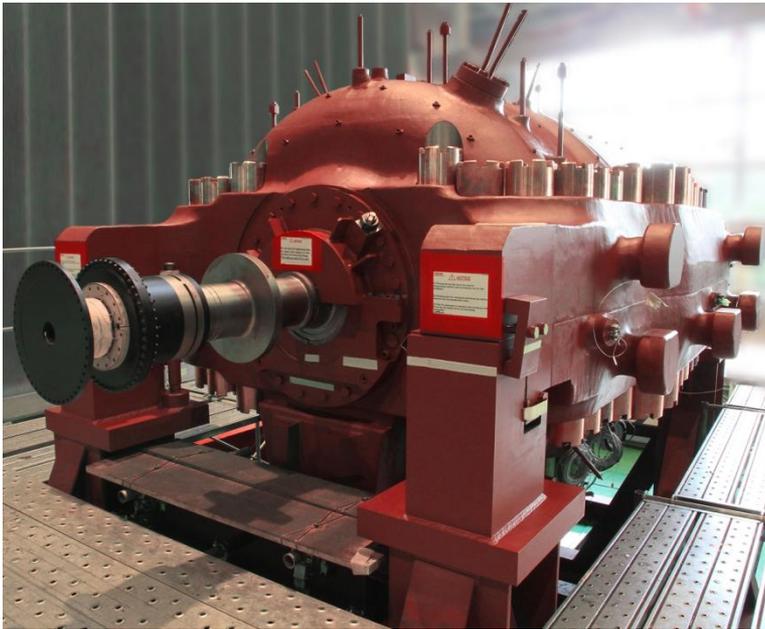


*Below: Rotor and Outer Casing of Demonstration Turbine (Courtesy: Toshiba)*



- Fusion of a USC steam turbine (double casing design) with the design of gas turbine (cooled and coated blades). The inner casing is internally cooled.
- NG and oxidant mixture of 20% O<sub>2</sub> & 80% CO<sub>2</sub> is mixed with 700°C recycle CO<sub>2</sub> to provide a turbine inlet temperature of 1150°C at 300 bar
- 5MW combustor test with 700°C oxidant flow confirmed calculated performance. Diffusion flame, no premixing gives stable combustion conditions.
- 200MWth turbine unit scaled to 50MWth by partial arc admission to the turbine blades, minimizing risk for the commercial-scale turbine
- The use of pure O<sub>2</sub> means very low NO<sub>x</sub> formation. Trace NO<sub>x</sub> will be formed from fuel-derived N<sub>2</sub> in the natural gas.

# The high pressure CO<sub>2</sub> turbine

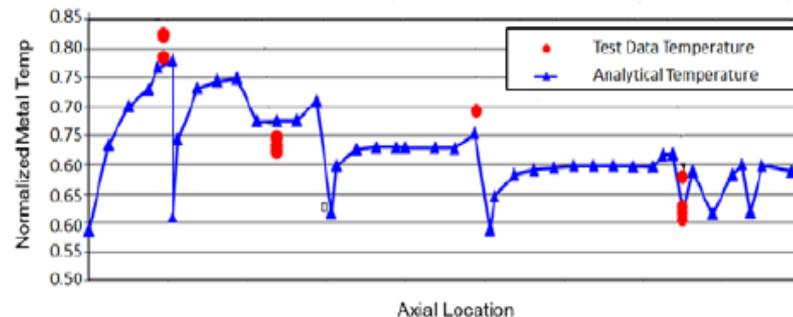
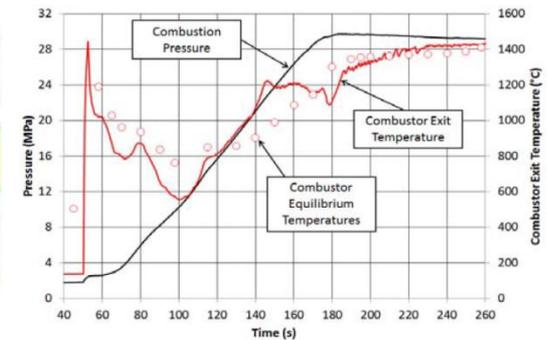
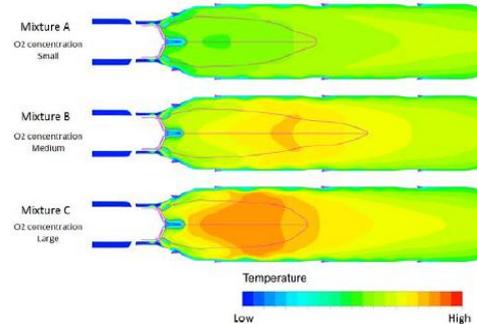
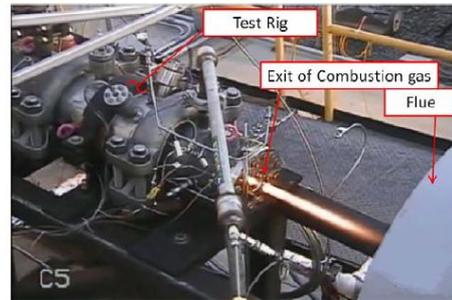


# NET Power 5Mw first combustor test

Combustion tests under these conditions have been underway by Toshiba since 2013.<sup>1</sup>

Tests have been conducted under various pressures and CO<sub>2</sub>/O<sub>2</sub> ratios all of which were successful and agreed with theoretical models.<sup>1</sup>

Additionally combustor metal temperatures matched well with predictive models.<sup>1</sup>



1. Iwai, Y., Itoh, M., Morisawa, Y., Suzuki, S., Cusano, D., & Harris, M., "Development Approach to the Combustor of Gas Turbine for OXY-fuel, Supercritical CO<sub>2</sub> Cycle", Proceedings of ASME Turbo Expo, 2015, GT2015-43160

# The High Pressure Combustor Test Vessel

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# HEATRIC DIFFUSION BONDED PLATE FIN HEAT EXCHANGER

Plates have chemically etched channels and are stacked then diffusion bonded

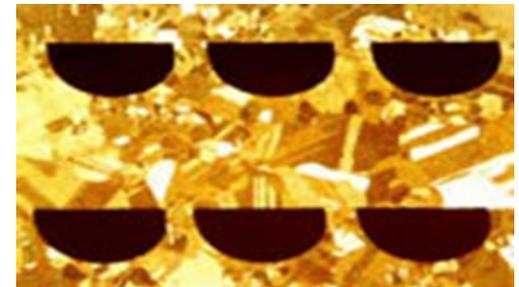
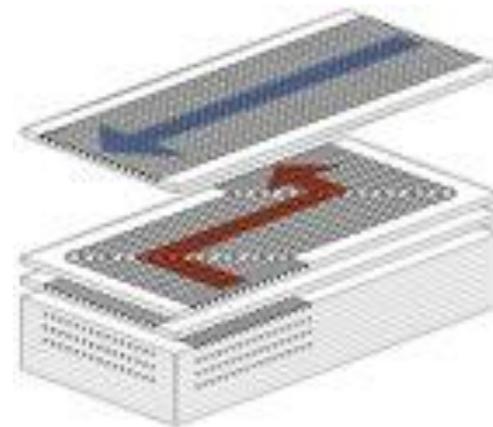
Grain growth occurs between plates during the diffusion bonding process

Very compact and potentially low cost system

Headers welded to the outside of the blocks

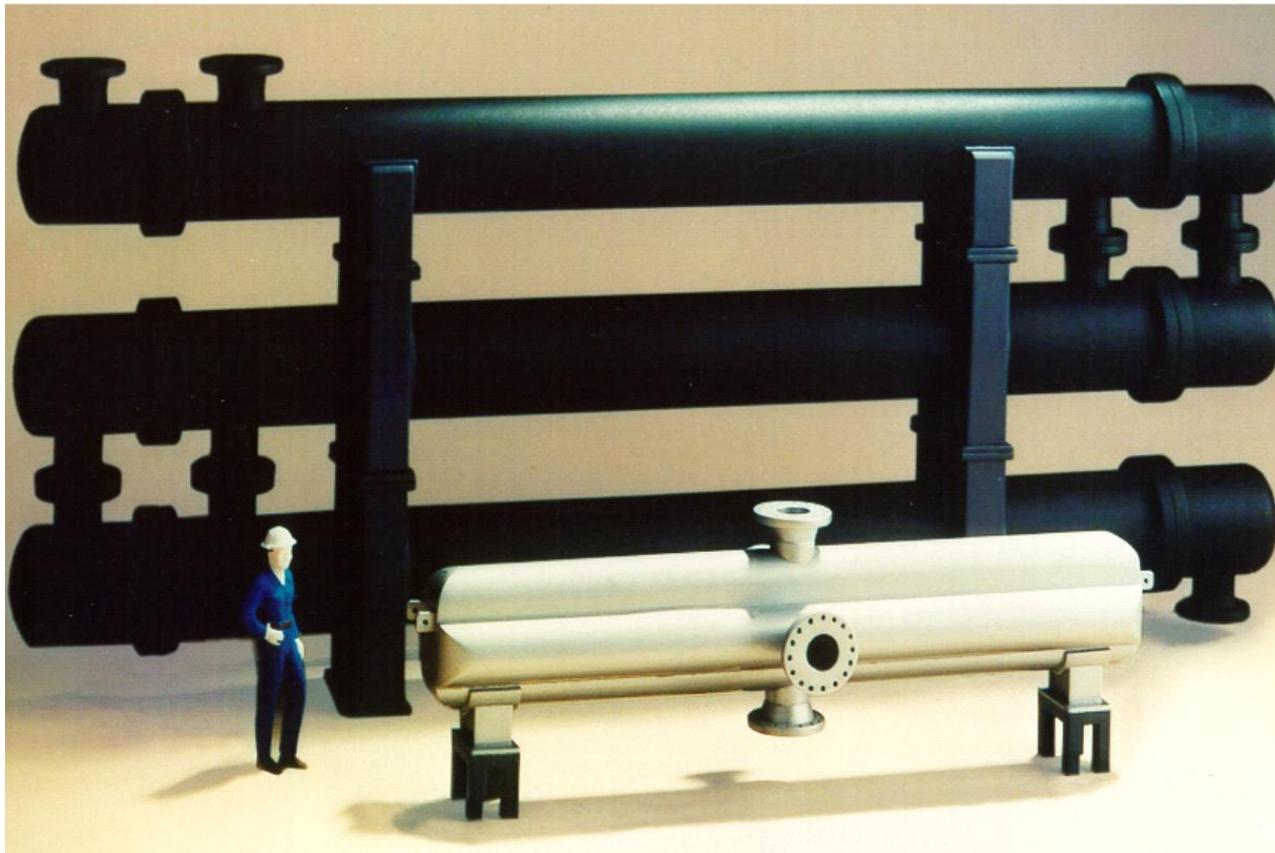
Multiple blocks welded to form batteries

617 alloy allows operation at  $>300\text{bar}$  and  $>700^\circ\text{C}$



# Size and Weight Savings

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# NET Power is near-term deployable – HX

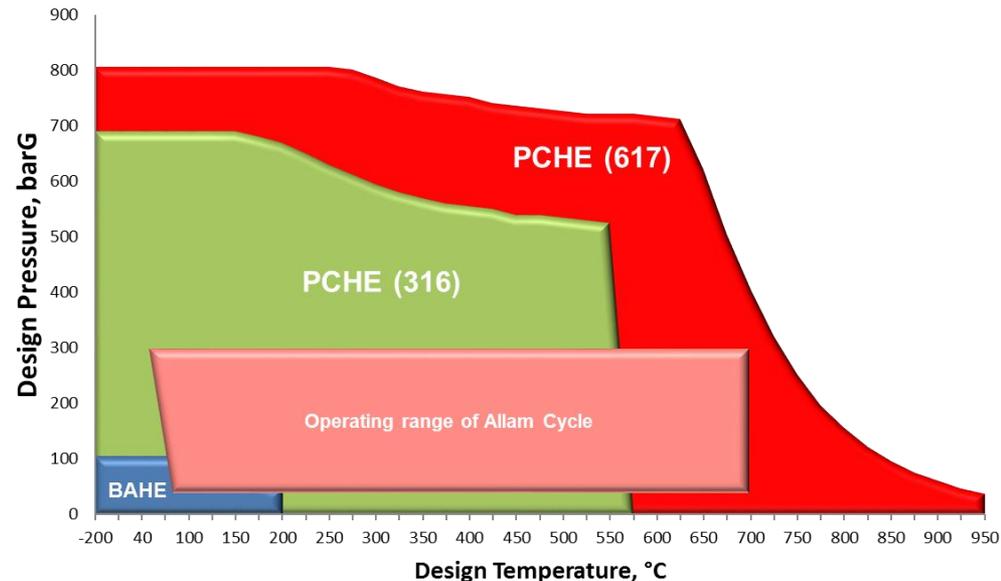
Heat exchanger design is well within Heatric's capabilities

- NP has been discussing recuperators with other manufacturers as well.

HX designed following ASME guides:

- ASME Sec. IID - function of design temperature.
- ASME Sec. VIII, DIV. 1 - pressure vessel design code
- ASME Sec. III NH, DIV. 2 - fatigue and creep in high temperature (developed for nuclear power generation extreme conditions).

Design of HX train limits nickel alloys to only hottest section, 316 (lower cost material) can be used for the majority while maintaining strength and corrosion resistance



# Main Process Heat Exchanger

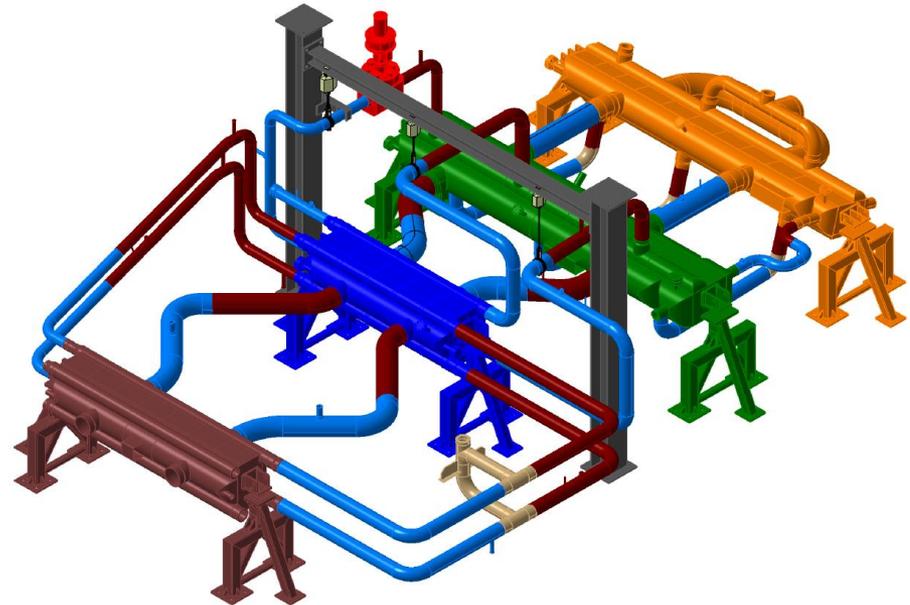
- The demonstration Printed Circuit Heat Exchanger has been supplied by Heatric
- Large SA/V allows for high P & T operation with tight approach.
- Stacks of 1.6mm thick plates are photo masked then chemically etched to produce complex passage arrangements
- The plates are diffusion bonded at high T to form a homogeneous monolithic block.
- The main recuperator operates over a range from 50°C to 705°C . It has a multi-stream configuration in 4 sections
  - 617 alloy for T > 550°C
  - 316L alloy T < 550°C.
- The demonstration recycle compressor aftercooler is also PCHE type



Low Temperature Section



Aftercooler being lowered into position



Demonstration plant main process heat exchanger network (Courtesy: Heatric)

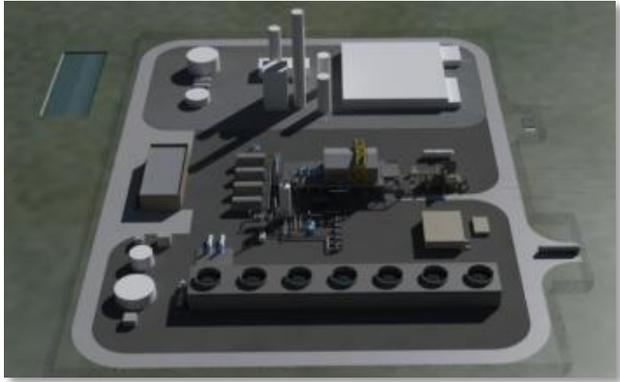
# Part of the recuperative heat exchanger battery and the recycle CO<sub>2</sub> high pressure pump



# Direct contact cooler for turbine discharge gas and the CO<sub>2</sub>/O<sub>2</sub> oxidant compressor



# The 300MWe Commercial Natural Gas Plant is Currently in Pre-FEED Design



- A detailed pre-FEED design study is underway.
- Major equipment is in an advanced stage of readiness:
  - **Turbine and Combustor:** The demonstration turbine size allows verification of the design for the 526 MWth commercial turbine.
  - **Heat Exchanger:** increase in size and quantity of cores for the commercial system.
  - **ASU:** The 3627 MT/day, 99.5% O<sub>2</sub> ASU has been demonstrated at this size by all major suppliers.
  - **Compressors:** The physical linkage of the CO<sub>2</sub> compressor and turbine is within the size capability of major compressor vendors.
  - **Pumps:** The multistage CO<sub>2</sub> pumps are demonstrated at the design duties required.

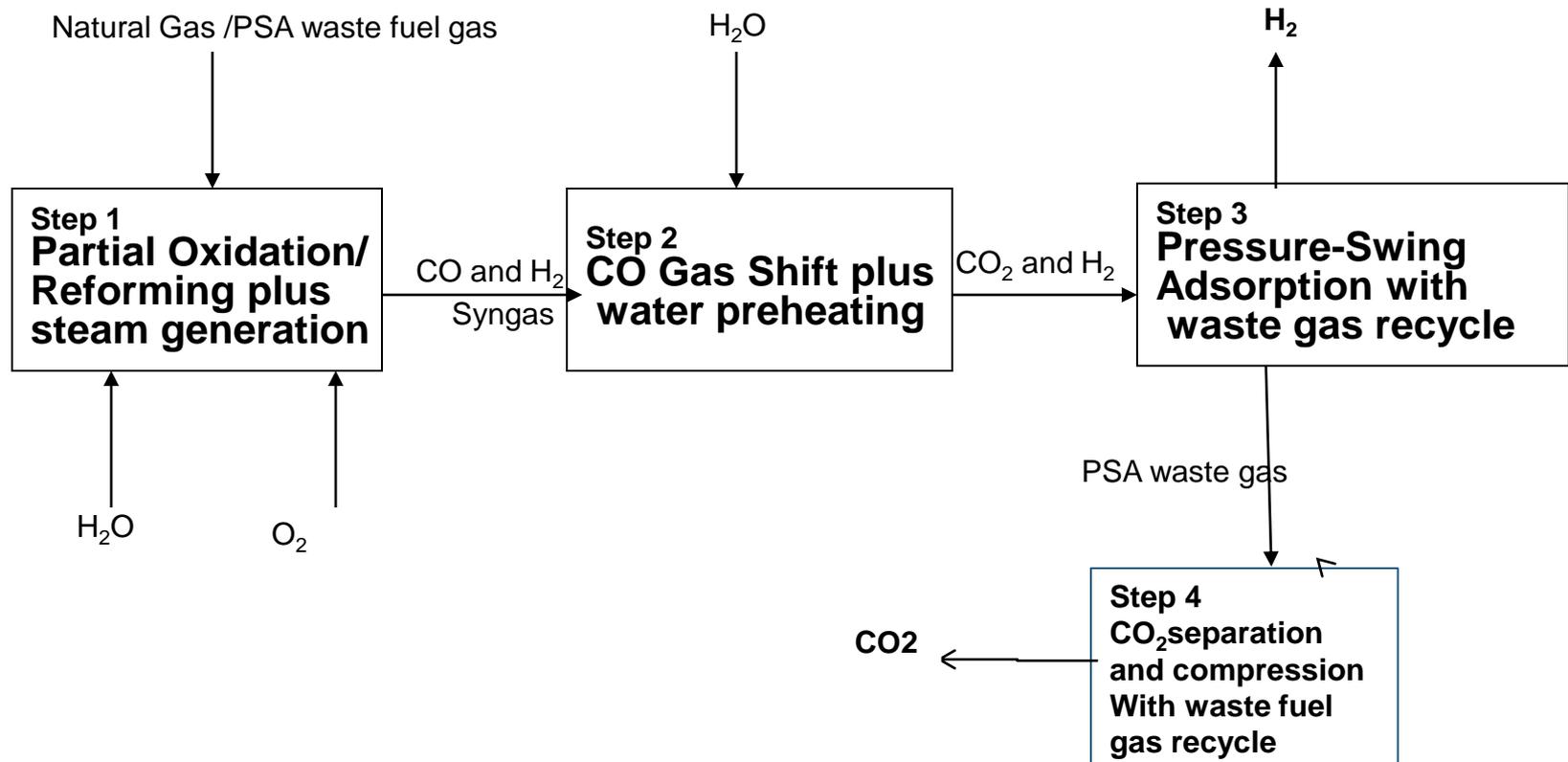
## NET Power 300 MWe Commercial Plant (CH<sub>4</sub> fuel)

Net power output	300 MW at ISO Conditions
Natural gas thermal input	526MW
LHV Efficiency	57.0%
Oxygen consumption	3627 MT/day (contained)
CO <sub>2</sub> Produced	2494 MT/day at 150 bar
Turbine outlet flow	923 kg/s
Turbine inlet condition	300 bar at 1158°C
Turbine outlet condition	30 bar at 727°C (approximately)

Excellent performance at high ambient conditions: 31C Air, 289 MW net

# Hydrogen Production Process Overview

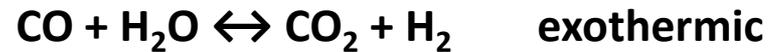
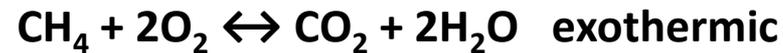
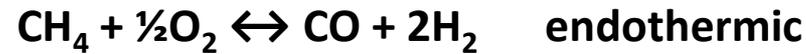
A Proven pressurized Process That Converts Natural Gas Oxygen and Steam to Hydrogen



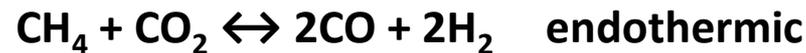
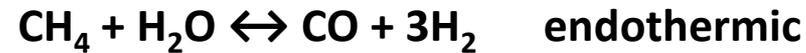
# Hydrogen Production Reactions

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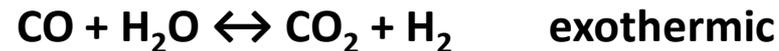
## Partial Oxidation



## Convective Heat Reforming

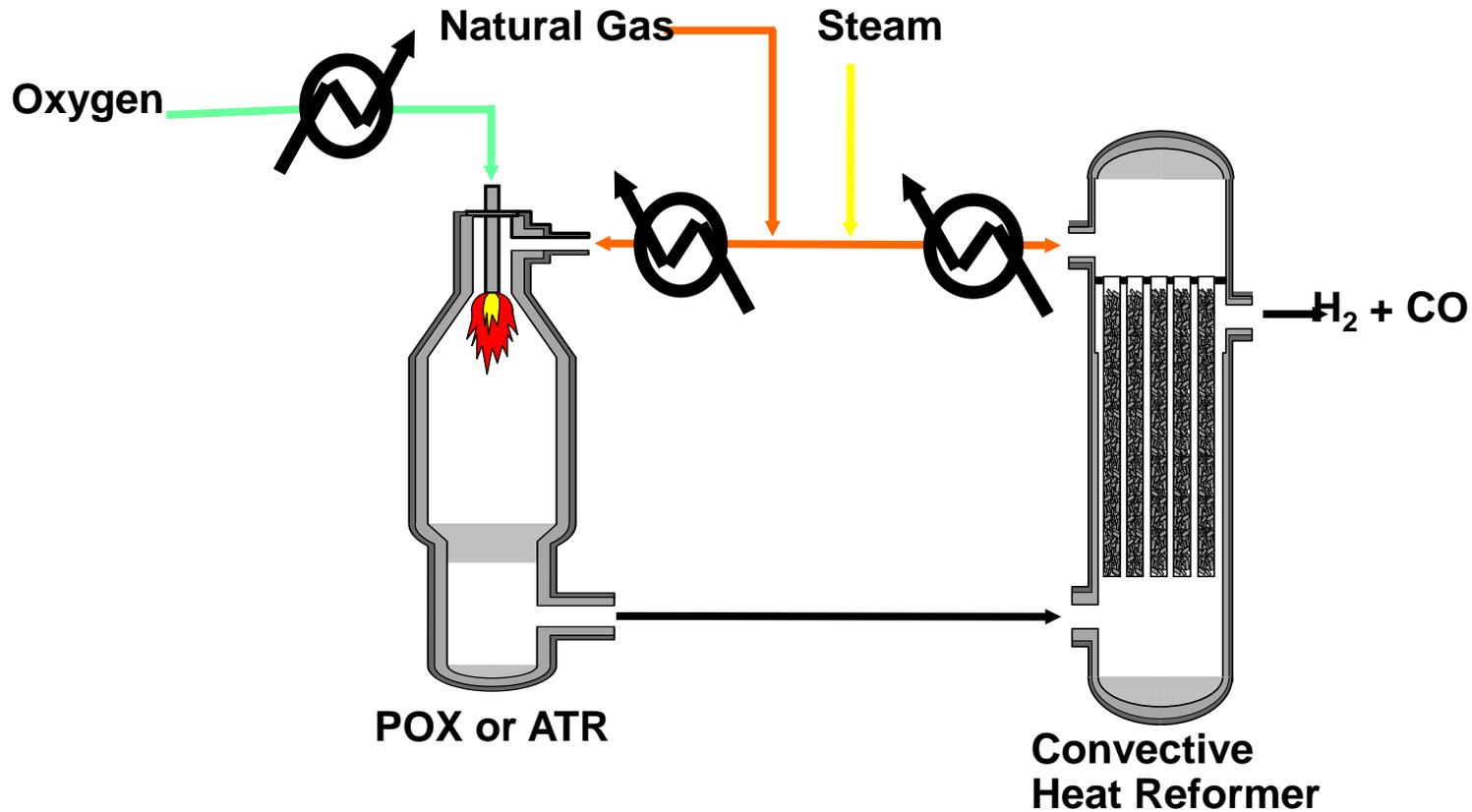


## Water-Gas Shift

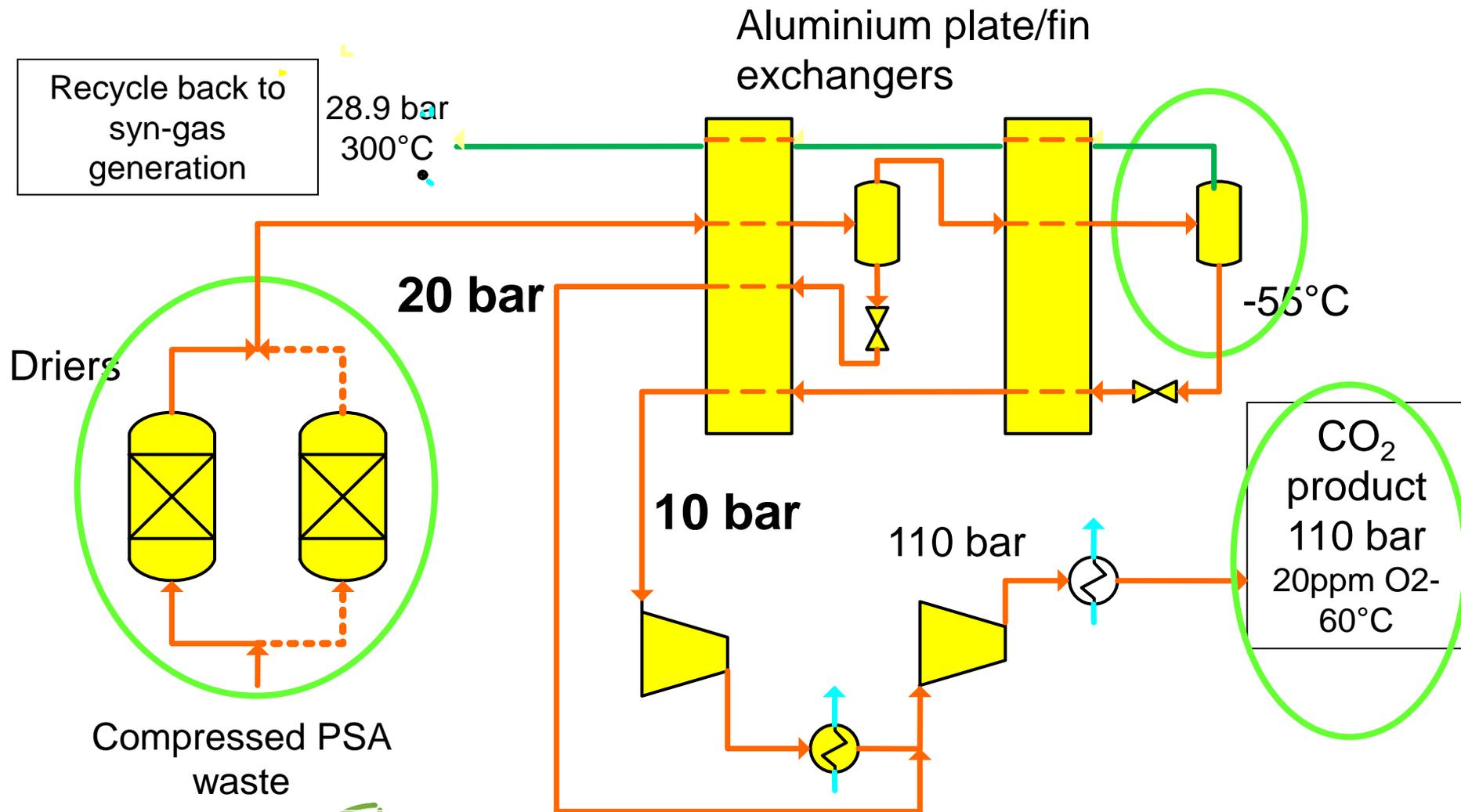


# Syn-gas System For Hydrogen Production

H<sub>2</sub> can be produced at up to 90bar pressure



# Low temperature CO<sub>2</sub> removal by condensation near the triple point



# GE F Class Turbines For Hydrogen Power

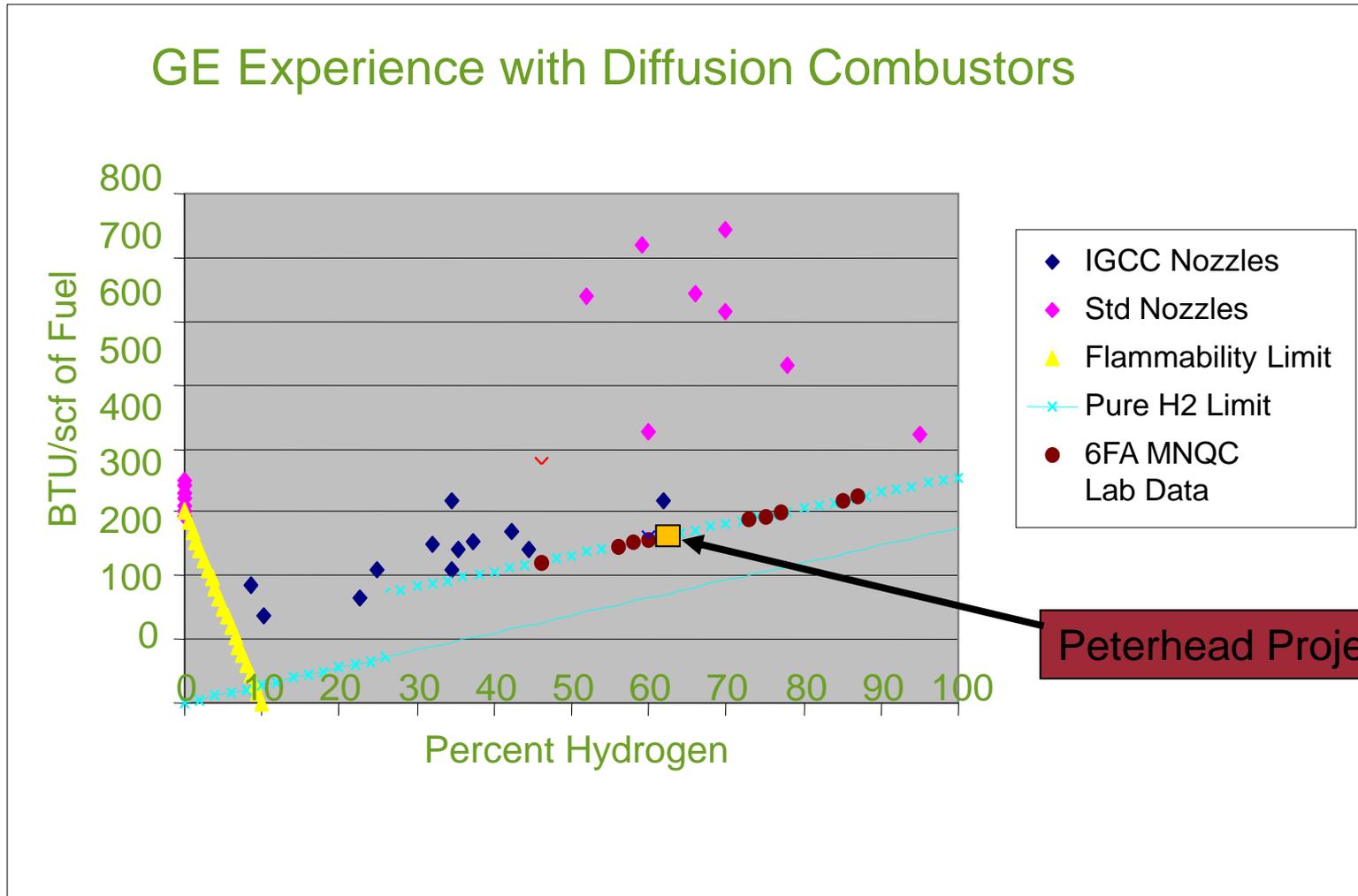
GE F Class Turbines Have Over 30 Million Hours Of Operations, the Largest, Most Experienced Fleet of High Efficiency Gas Turbines



	PSI Wabash	Tampa Polk	Exxon Singapore	Motiva Delaware
Turbine	7FA	7FA	2x6FA	2x6FA
H <sub>2</sub> (% vol)	24.8%	37.2%	44.5%	23.0%
LHV (BTU/ft <sup>3</sup> )	209	253	241	248
H <sub>2</sub> /CO Ratio	0.63	0.80	1.26	0.65
Diluent	Steam	N <sub>2</sub>	Steam	H <sub>2</sub> O/N <sub>2</sub>

Feasibility of high H<sub>2</sub> fuel combustion with low emissions has been demonstrated at F class conditions using proven syngas combustor design; reliability, availability and maintainability can be equivalent to natural gas turbines

# GE Hydrogen Combustion Experience GE data



# INTEGRATED POWER SYSTEM WITH AN ALLAM CO<sub>2</sub> CYCLE PLUS A HYDROGEN FUELED COMBINED CYCLE

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ALLAM cycle integrated with a GE PG9371(FB) combined cycle power system

Stand alone ALLAM cycle net power output                      290Mw

Stand alone GE PG9371(FB)

Combined cycle net power output                                      432.25Mw

Gas turbine fuel is 50% H<sub>2</sub>+50% N<sub>2</sub> molar concentration

Total net power output      697Mw              Cycle efficiency (LHV)      50.9%

CO<sub>2</sub> production (100% capture) at 150bar pressure      6437Metric tons per day

O<sub>2</sub> consumption (99.5% purity)                                      4979Metric tons per day

Approximate capital cost erected £1150/kw installed net capacity

net electricity cost                                      4.53pence/Kwhr

Capital charges plus operations 17%/year, Natural gas £5/million BTU (LHV), 8000hr/year, CO<sub>2</sub> credit £25/metric ton,

# Commercial Hydrogen Fuelling Installations

BP, Singapore



Air Products' Hydrogen Fuelling Systems



Supplied to major oil companies

8 RIVERS



Shell, Washington, DC, USA

# Underground Liquid Hydrogen Fuelling Tank – Washington, DC, USA



# Liquid Hydrogen Tanker

capacity 3600 kg liq H<sub>2</sub>



# Oxy-fuel Technology for CO<sub>2</sub> Capture - Definition:

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**Fuel + oxygen with nitrogen rejected in an air separation plant**

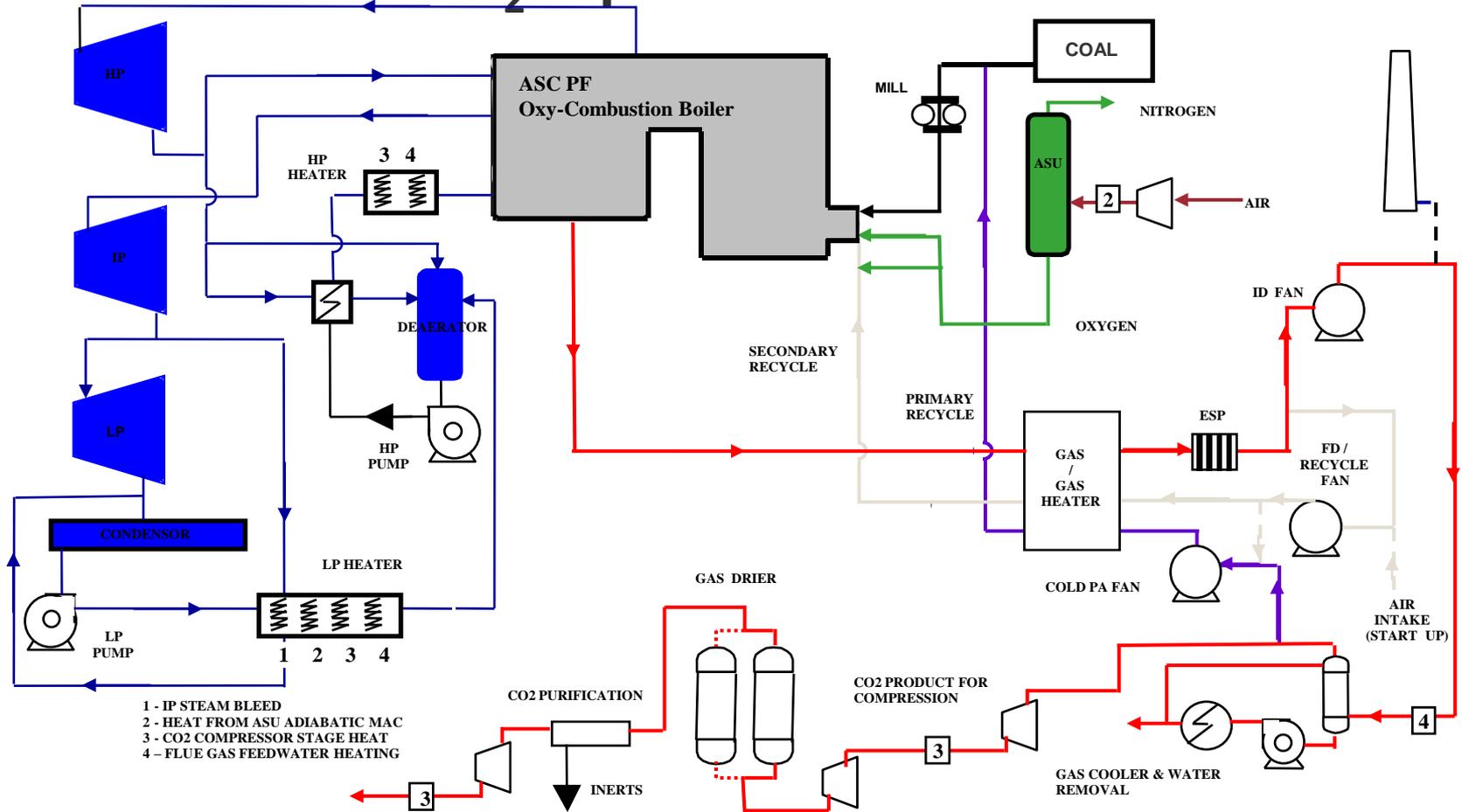
**Diluent flow of CO<sub>2</sub> or H<sub>2</sub>O or recycled flue gas with fuel to oxygen concentration ratio controlling combustion temperature**

**Independent control of heat output and combustion temperature**

**Low power consumption 95% O<sub>2</sub> plants and simple SOX and NOX removal**

**Minimal existing boiler and turbine plant modification.  
Demonstrated burner operation. Low risk system**

# Schematic of Supercritical PF Oxyfuel Power Plant With CO<sub>2</sub> Capture



# NO<sub>x</sub> and SO<sub>2</sub> Reactions in the CO<sub>2</sub> Compression System

SO<sub>2</sub>, NO<sub>x</sub> and Hg can be removed in the CO<sub>2</sub> compression process, in the presence of water and oxygen.

SO<sub>2</sub> is converted to Sulphuric Acid, NO<sub>2</sub> converted to Nitric Acid:

- $\text{NO} + \frac{1}{2} \text{O}_2 = \text{NO}_2$  (1) Slow
- $2 \text{NO}_2 = \text{N}_2\text{O}_4$  (2) Fast
- $2 \text{NO}_2 + \text{H}_2\text{O} = \text{HNO}_2 + \text{HNO}_3$  (3) Slow
- $3 \text{HNO}_2 = \text{HNO}_3 + 2 \text{NO} + \text{H}_2\text{O}$  (4) Fast
- $\text{NO}_2 + \text{SO}_2 = \text{NO} + \text{SO}_3$  (5) Fast
- $\text{SO}_3 + \text{H}_2\text{O} = \text{H}_2\text{SO}_4$  (6) Fast

**Rate of Reaction 1 increases with Pressure to the 3<sup>rd</sup> power**

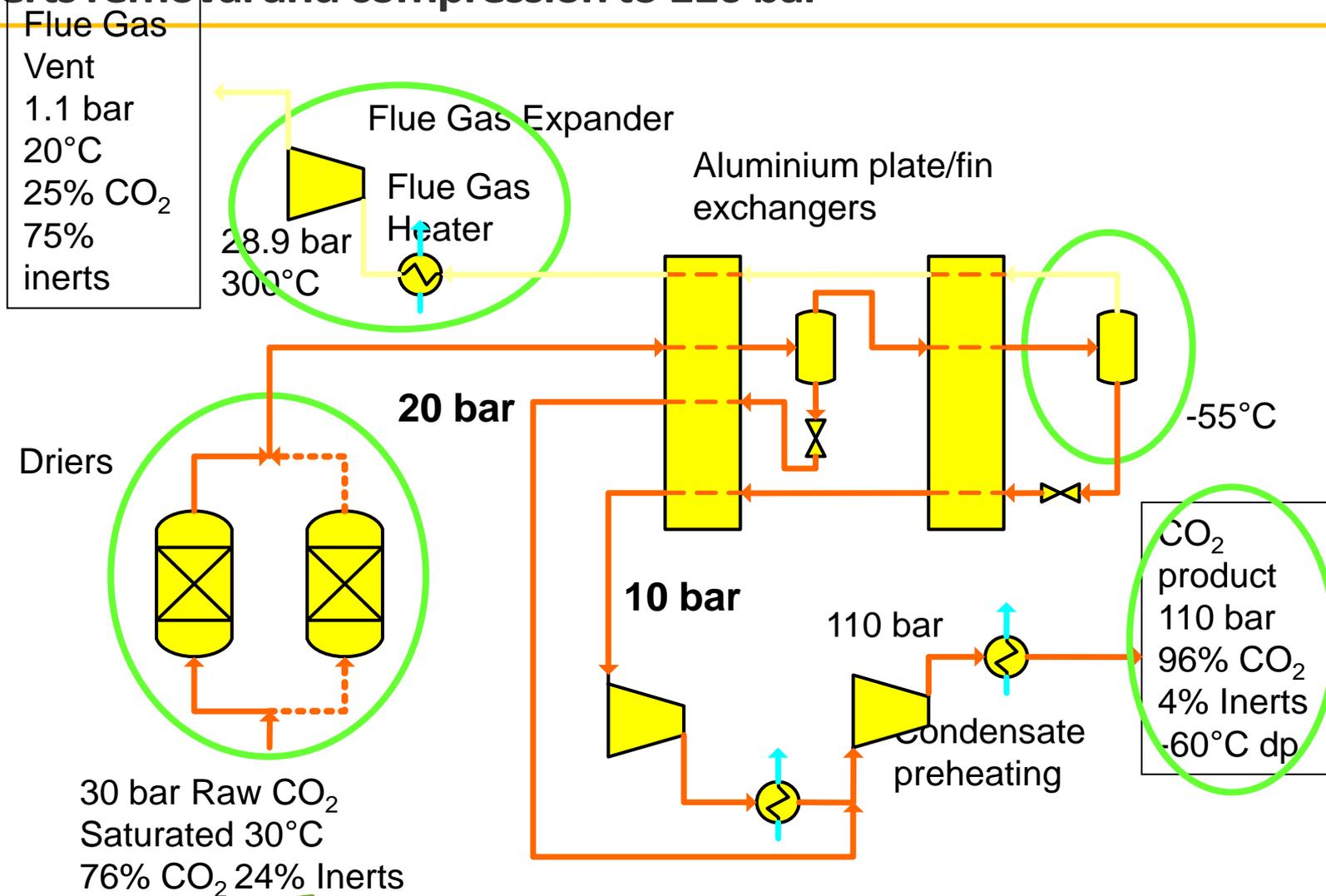
- only feasible at elevated pressure. Adiabatic CO<sub>2</sub> compression to 15bar with heat to BFW is economic.

**No Nitric Acid is formed until all the SO<sub>2</sub> is converted**

**Pressure, reactor design, residence times, and NO concentration (>100ppm) are important**

**H<sub>2</sub>SO<sub>4</sub> >25% concentration converted to gypsum**

# CO<sub>2</sub> Compression and Purification System – Inerts removal and compression to 110 bar



# CONCLUSIONS

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- **Cost of electricity from the Allam cycle using natural gas fuel with 100% CO<sub>2</sub> capture is about the same as the best NGCC system with no CO<sub>2</sub> capture.**
- **CO<sub>2</sub> is produced as either a high pressure fluid for pipeline transportation or as a liquid for shipping in tankers.**
- **Cost of electricity using the coal based Allam cycle with 100% CO<sub>2</sub> capture is about 17% lower than a 600°C, 300bar steam cycle with no CO<sub>2</sub> capture.**
- **The demonstration Allam cycle plant at Laporte USA is currently nearing full power operation.**
- **Hydrogen can be produced at up to 90 bar pressure with 100% CO<sub>2</sub> capture at an efficiency of over 75%, comparing the lower heating value of H<sub>2</sub> product and natural gas feed.**
- **Hydrogen fuel for gas turbines and fuel cells for vehicles and decentralised power with 100% CO<sub>2</sub> capture.**
- **Hydrogen production can be integrated with large scale Allam cycle power production**
- **OXY-FUEL conversion of existing coal fired power stations offers low risk option for dealing with existing CO<sub>2</sub> emission.**